

# **Commercial Development of Terbium-Based Giant Magnetostrictive Alloys for Cryogenic Applications**

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# History

- 1965: Giant Magnetostriction measured in the basal planes of rare earth metals Terbium (Tb) and Dysprosium (Dy) at Naval Ordnance Lab (NOL) and Ames Laboratory, D.O.E.  
Strains approaching 1% (10,000 ppm) at low temperatures persist at the 0.6% (6000 ppm) level up to about 150 K
- 1970's: Room Temperature Giant Magnetostrictive TERFENOL-D developed at NOL

- 1980: Processes to produce high performance transducer elements from these alloys developed at Ames Laboratory
- 1986: Commercial volume production of TERFENOL-D by ETREMA Products, Inc.
  - $\text{Tb}_x\text{Dy}_{1-x}\text{Fe}_{1.9-1.95}$ ,  $x=0.35$  to  $0.27$
  - Rare Earth Metals Tb (Terbium) and Dy (Dysprosium) alloyed with Fe (Iron)

- 1990's: Cryogenic alloys researched

- $\text{Tb}_x\text{Dy}_{1-x}$  Single crystals of hexagonal close-packed (hcp) Binary Solid Solution Alloys

- $\text{Tb}_x\text{Dy}_{1-x}\text{Zn}$  Single Crystals of body-centered cubic (bcc) Intermetallic Compounds (in progress)

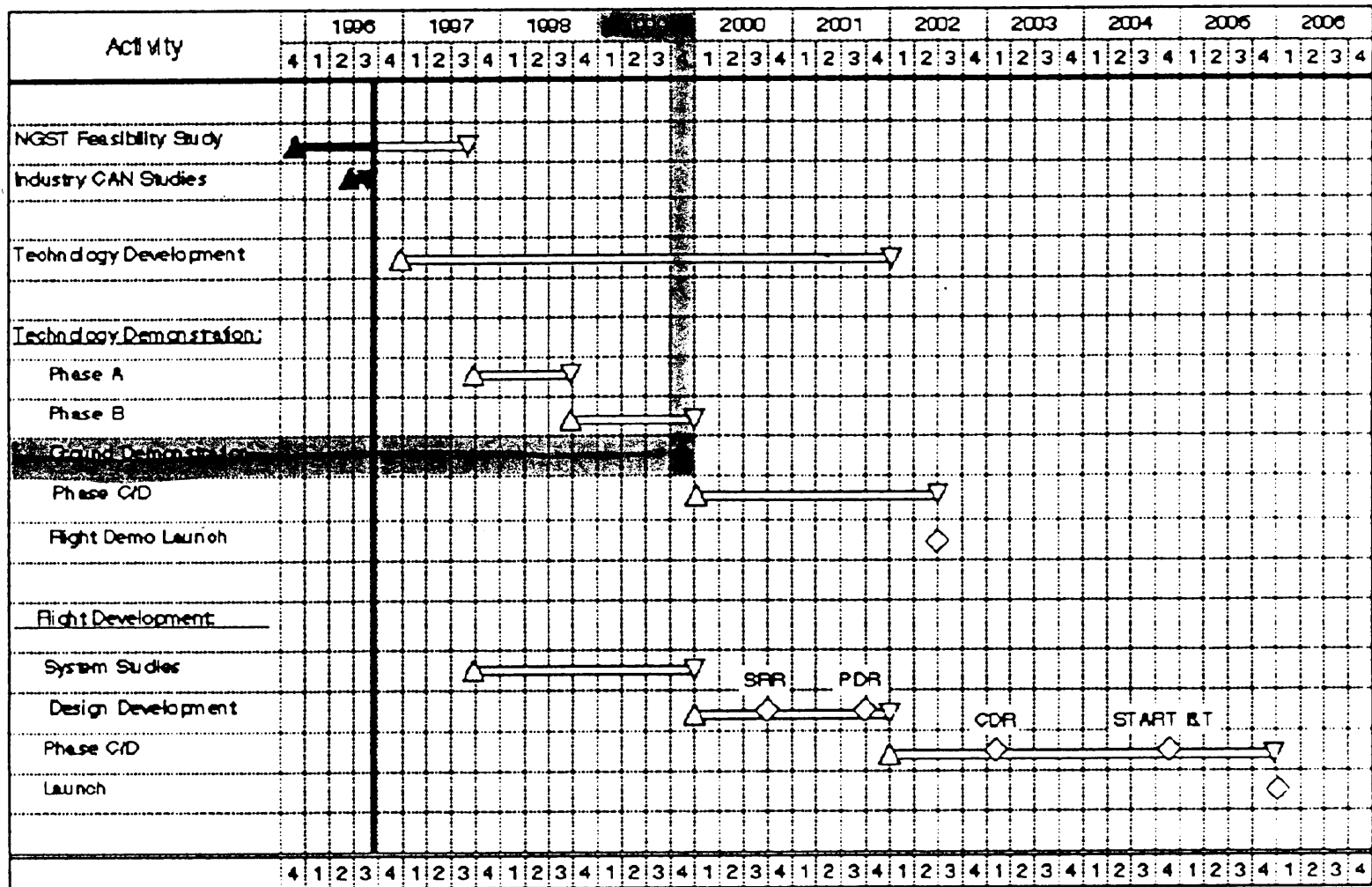
- $\text{Tb}_x\text{Dy}_{1-x}\text{Fe}_{1.9-1.95}$  (TERFENOL-D) where  $x=1.0$  to 0.4 face-centered cubic (fcc) Laves phase Intermetallic compounds (in progress)

# Needs

- Increasing number of potential applications for actuation at cryogenic temperatures but materials are not available
- NGST Mirror Manipulators will require commercial quantities of cryogenic materials but processes are not developed
- Major effort needed to develop commercial volume processes in time to meet NGST scheduled demonstration in 4th quarter 1999.

# NGST

## NGST Schedule



# Status

## WHAT HAS BEEN ACCOMPLISHED TO DATE

- TERFENOL-D,  $\text{Tb}_x\text{Dy}_{1-x}\text{Fe}_{1.9-1.95}$ , where  $x=0.4$  to  $0.27$ , stoichiometries used in devices operating in the  $-60^\circ\text{C}$  to  $100^\circ\text{C}$  range.
  - Large-scale production capabilities at ETREMA
    - Near-single crystal  $\langle 112 \rangle$  crystallographic direction aligned along the drive axis produced by the free stand zone melt (FSZM) crystal growth method with diameters between 2 and 7 mm and lengths of 250 mm
    - $\langle 112 \rangle$  directionally solidified large diameter (10 mm to 65 mm) drivers produced by the modified Bridgman (MB) method in lengths of 380 mm

- $\text{Tb}_x\text{Dy}_{1-x}$  hcp binary alloys

- Research quantities prepared by the strain anneal process. Size limited and required c-axis perpendicular to the drive axis not controllable. Low yields, short lengths and excessive waste due to required machining.

- Moderate success in preparing some aligned polycrystalline sheets by hot rolling and subsequent anneal. Sacrifice in strain (65% of the single crystal strain attained) considered excessive; process not economical on large scale.



- $\text{Tb}_x\text{Dy}_{1-x}\text{Zn}$  bcc Intermetallic Compounds

- Early success in growing preferred  $\langle 100 \rangle$  oriented single crystals in sealed crucibles by the Bridgman method

- Attempts to increase crystal size have not been successful in the laboratory and research is in progress at the Ames Laboratory and NSWCCD to grow and characterize these crystals

# ETREMA's PROPOSED APPROACH TO COMMERCIAL DEVELOPMENT

- TERFENOL-D,  $\text{Tb}_x\text{Dy}_{1-x}\text{Fe}_{1.9-1.95}$ , where  $x=1.0$  to  $0.4$ 
  - To be useful at cryogenic temperatures (30 K and below), the terbium content in TERFENOL-D must be increased
  - The Tb-Fe and Dy-Fe binary phase diagrams show that  $\text{TbFe}_2$  is more peritectic in nature, which complicates the crystal growth/directional solidification processes currently used to produce high performance Dy-rich ( $x=0.4$  to  $0.27$ ) drive elements

- The critical parameters for crystal growth need to be developed for the higher Tb/Dy ratio ( $x=1.0$  to  $0.4$ ) materials.
- These alloys could produce strains as high as 5,000 ppm at 30 K, most of which is achieved at practical applied fields ( $H=1$  to  $2$  kOe).

- $\text{Tb}_x\text{Dy}_{1-x}$  hcp binary solid solution alloys
  - The reactive nature of the rare earths in their molten state dictates the single crystal growth from the melt by a containerless method.
  - The current strain anneal method is a solid state process which lacks control of the preferred crystallographic (a-axis or b-axis) direction along the drive axis.
  - ETREMA proposes to develop the process to produce these c-axis perpendicular drivers in a controlled manner.

- The largest known magnetostrictions exist in the  $\text{Tb}_x\text{Dy}_{1-x}$  system with strains between 9000 ppm and 6000 ppm achieved in the 0 K to 150 K temperature range.
- Individual drivers are useful for compressive loads up to 25 MPa.
- They can be bundled in laminated form to increase the projection area and extend the frequency range of operation.
- Low hysteretic and low eddy current loss transduction

- $\text{Tb}_x \text{Dy}_{1-x} \text{Zn}$  bcc intermetallic compounds
  - Metallurgical challenge in formation of homogeneous alloys due to high vapor pressure of Zn.
  - Seeded Bridgman crystal growth method being developed at Ames Laboratory with characterization at NSWCCD.
  - ETREMA plans to scale up the process after completion of this R&D effort.
  - $\langle 100 \rangle$  crystallographic oriented single crystals to be produced with easy axis controlled by varying  $x$  between 0 and 0.4 in the  $\text{Tb}_x \text{Dy}_{1-x} \text{Zn}$  system.

- Large strains between 4500 ppm and 6500 ppm can be achieved at low applied fields, with loads up to 60 MPa 0 K to 150 K temperature range.

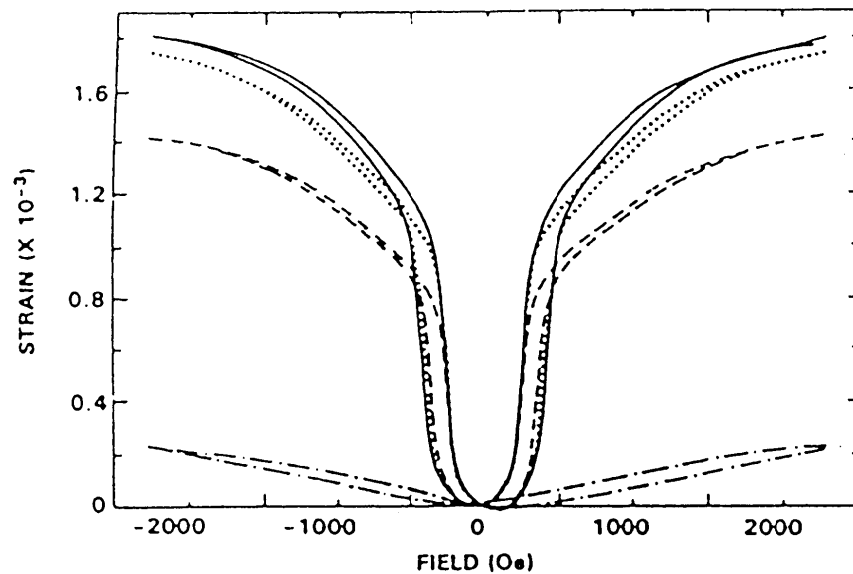


Fig. A. Magnetostriction curves of  $\text{Tb}_{0.3}\text{Dy}_{0.7}\text{Fe}_{1.9}$  at 13.3 MPa compressive stress  $-50^\circ\text{C}$  (dot-dashed curve), and  $0^\circ\text{C}$  (solid curve),  $20^\circ\text{C}$  (dotted curve), and  $80^\circ\text{C}$  (dashed curve)

Clark, Teter, and McMasters, *J. Appl. Phys.*,  
Vol. 63, No. 8, 15 April 1988

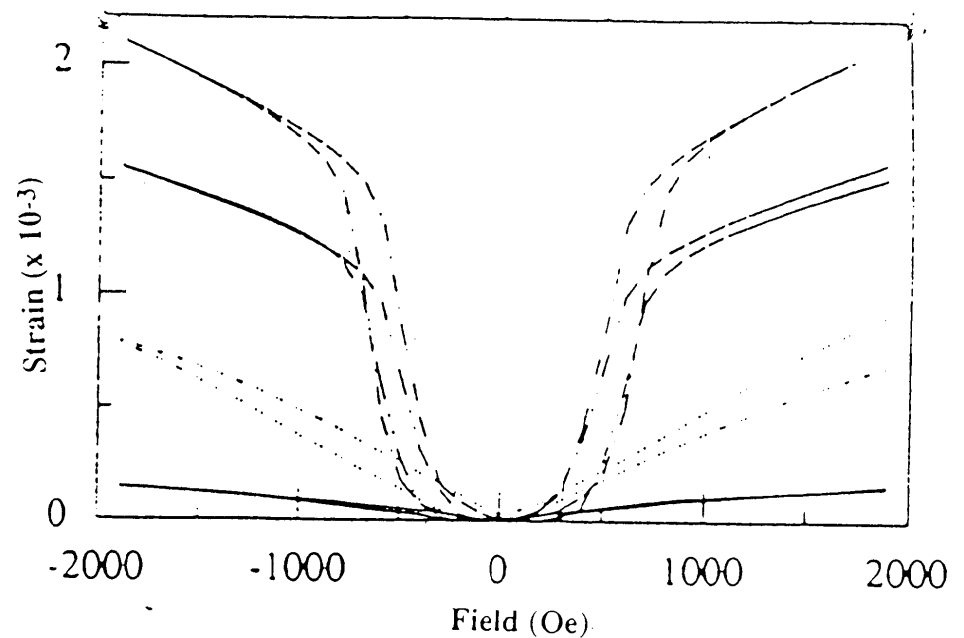


Fig. B. Magnetostriction of  $\text{Tb}_{0.35}\text{Dy}_{0.65}\text{Fe}_{1.9}$  under a compressive stress of 15.7 MPa: (a)  $-196^\circ\text{C}$  (solid curve), (b)  $-116^\circ\text{C}$  (dotted curve), (c)  $-68^\circ\text{C}$  (dot-dashed curve), and (d)  $+24^\circ\text{C}$  (dashed curve).

Clark, Teter, and Wun-Fogle, *J. Appl. Phys.* Vol. 69,  
No. 8, 15 April 1991



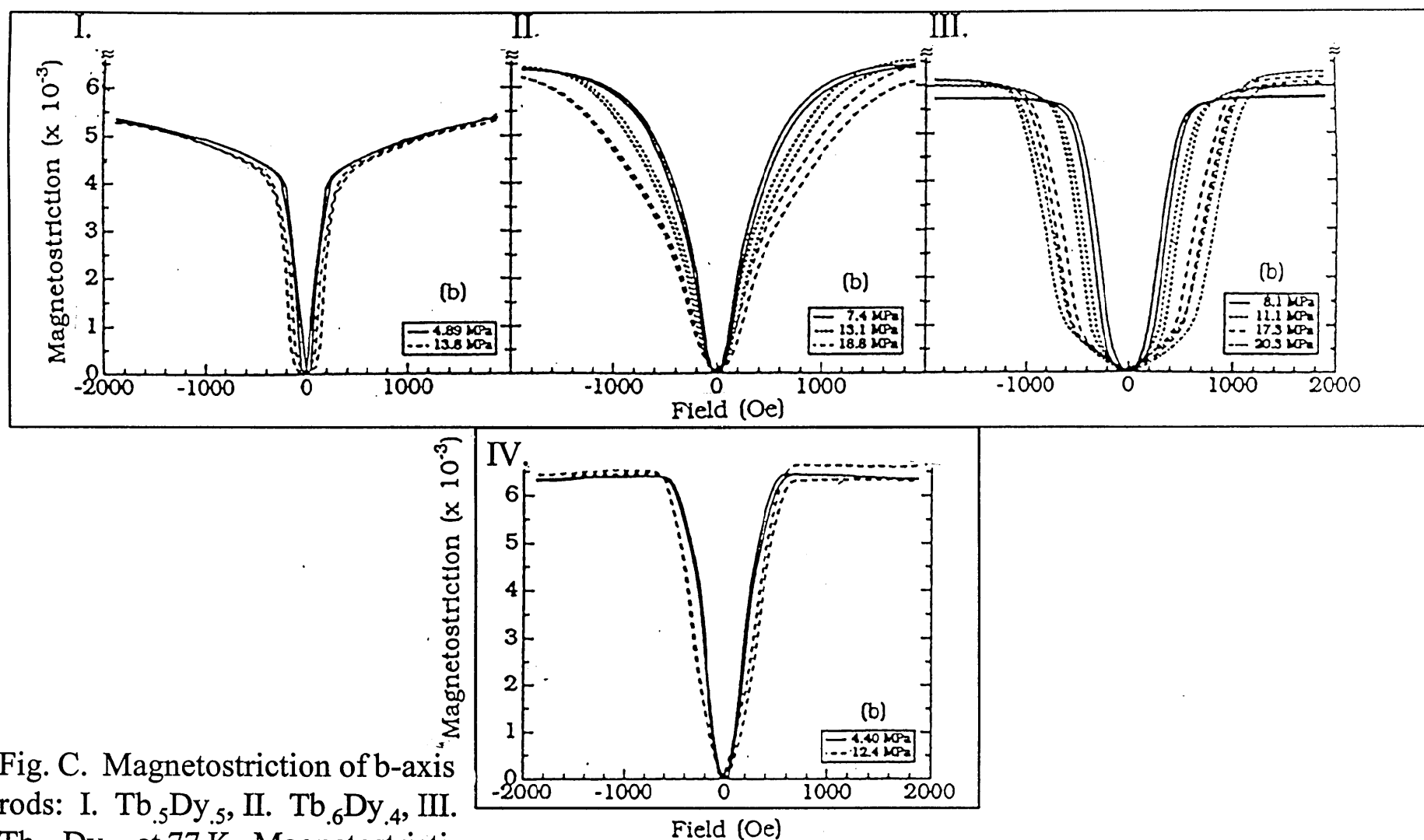


Fig. C. Magnetostriction of b-axis rods: I. Tb<sub>0.5</sub>Dy<sub>0.5</sub>, II. Tb<sub>0.6</sub>Dy<sub>0.4</sub>, III. Tb<sub>0.67</sub>Dy<sub>0.33</sub> at 77 K. Magnetostriction of an a-axis rod: IV. Tb<sub>0.6</sub>Dy<sub>0.4</sub> at 77 K.

A.E. Clark, M. Wun-Fogle, J.B. Restorff and J.F. Lindberg,  
*IEEE Trans. on Magnetics*, 28, No.5. Sept. 1992 p.3156.

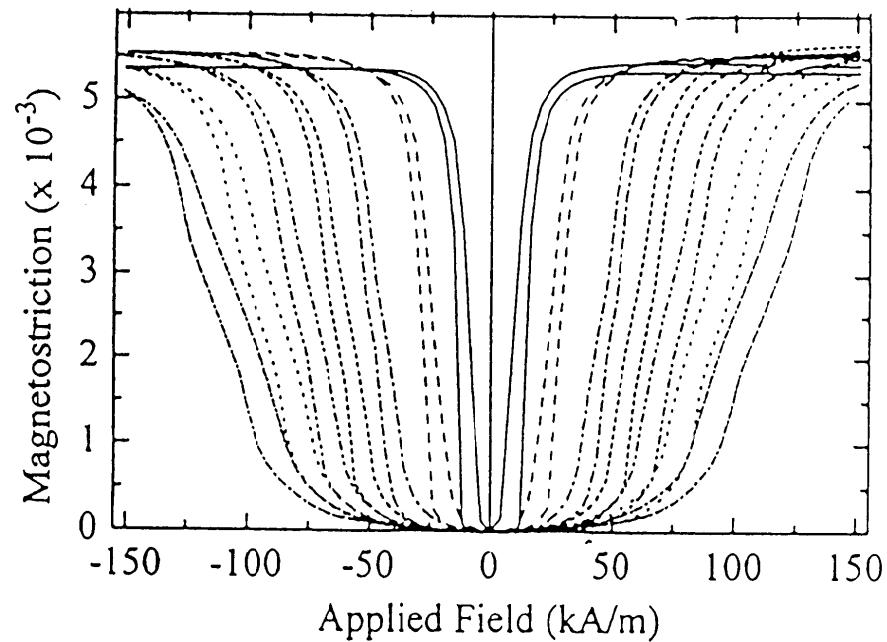


Fig. D. Magnetostriction of single crystal TbZn along the easy [100] axis at 77 K for compressive stresses of 5.3 MPa ———, 13.3 MPa — — —, 24.6 MPa ·····, 31.1 MPa - · - · - ·, 37.5 MPa ·····, 44.0 MPa ·····, 50.5 MPa ·····.

*A.E. Clark, J.B. Restorff, M. Wun-Fogle, J.F. Lindberg, Journal of Magnetism & Magnetic Materials 140-144 (1995) 1151-1152*